

LEVEL II

12

AD A060518

CAVITATION DYNAMICS:

III. THRESHOLDS AND THE GENERATION OF TRANSIENT CAVITIES

by

H. G. Flynn

The work described in this report was supported by the Office of Naval Research -Physics Program (Code 421) through Contract N00014-76-C-1080

DDC FILE COPY

25 July 1978

Acoustical Physics Laboratory
Department of Electrical Engineering
University of Rochester
Rochester, N. Y. 14627

DDC
RECEIVED
OCT 31 1978
D

Distribution of this document is unlimited.

DISCLAIMER NOTICE

**THIS DOCUMENT IS BEST QUALITY
PRACTICABLE. THE COPY FURNISHED
TO DTIC CONTAINED A SIGNIFICANT
NUMBER OF PAGES WHICH DO NOT
REPRODUCE LEGIBLY.**

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER None	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) CAVITATION DYNAMICS: III. THRESHOLDS AND THE GENERATION OF TRANSIENT CAVITIES.		5. TYPE OF REPORT & PERIOD COVERED 9 Technical rept.
7. AUTHOR(s) 10 H. G. Flynn		6. PERFORMING ORG. REPORT NUMBER None
9. PERFORMING ORGANIZATION NAME AND ADDRESS Acoustical Physics Laboratory, Dept. of Elec. Eng., University of Rochester, Rochester, N. Y. 14627		8. CONTRACT OR GRANT NUMBER(s) 15 N00014-76-C-1080
11. CONTROLLING OFFICE NAME AND ADDRESS Office of Naval Research (Code 421) Department of the Navy		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Physics Program, ONR
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) NA 12 L7p.		12. REPORT DATE 11 25 Jul 1978
		13. NUMBER OF PAGES 17
		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES To be submitted to Journal of the Acoustical Society of America		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Cavitation, acoustics, bubbles, cavitation dynamics, cavitation thresholds, cavitation activity, transient cavities		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Dynamics of small argon bubbles under the influence of an acoustic pressure field have been studied using a mathematical formulation derived previously (J. Acoust. Soc. 57, 1379-1396 (1975)). Calculation of the maximum pressure in a collapsing bubble and work done by expanding bubbles show there are two cavitation pressure thresholds -- one for the onset of cavi- tation activity and the other for a decrease in cavitation activity.		

401 344

LB

ACCESSION No.	
RTM	White Section <input checked="" type="checkbox"/>
NDG	Grey Section <input type="checkbox"/>
UNANNOUNCED	<input type="checkbox"/>
JUSTIFICATION	
BY	
RESTRICTION/AVAILABILITY 00000	
Dist.	Avail. order/ST. 00000
A	

CAVITATION DYNAMICS: III THRESHOLDS AND THE GENERATION OF TRANSIENT CAVITIES

by

H. G. Flynn

Department of Electrical Engineering
University of Rochester, Rochester, New York 14627

Phenomena associated with acoustic cavitation in liquids are observed to change abruptly in magnitude with small changes in the amplitude of the acoustic pressure or intensity. The amplitudes at which changes occur are called cavitation thresholds. Investigators have noted that, once such thresholds have been exceeded, the phenomenon being observed rises to a maximum and then decreases. L. D. Rozenberg¹ was perhaps the first to point out the existence of these maxima.

Many experimenters have determined both the existence and magnitude of cavitation thresholds, using erosion of solids, cavitation noise, chemical reactions and biological effects as the cavitation phenomena under observation.² The work of Kaufman, Miller, Griffiths, Ciaravino and Carstensen³ and of Clarke and Hill⁴ may be cited as examples of the use of biological effects in threshold measurements, while that of Neppiras and Coakley⁵ may be cited as an example of use of cavitation noise. For brevity, the term "cavitation activity" will be used to denote the wide range of phenomena associated with cavitation fields or zones and used by various experimenters to demonstrate the existence of thresholds as functions of pressure or intensity.

Attention will be limited here to the remarkable papers of Monakhov, Peshkovskii, Popovich, Fomichev, Chinyakov and Yakovlev⁶ and Brandt, Yakovlev and Peshkovskii⁷. These workers observed two cavitation thresholds -- one for the onset of cavitation activity and a second for a marked decrease in cavitation activity (except

for the radiation of noise). Monakhov et al distinguished three regimes of cavitation. Below the first threshold, there was no cavitation activity. Above the second threshold, cavitation activity (as evidenced by erosion, for example) virtually ceased, large bubbles were observed and the liquid resembled boiling water. Monakhov et al carried out their experiments at a single acoustic frequency (17.8 kHz) in water that presumably contained gas "seeds" or "nuclei" having a wide distribution of initial radii. In the terminology suggested by this author^{2,9} the first regime of Monakhov et al would be a zone containing only stable cavities while the regime bounded by the two thresholds would be a zone dominated by transient cavities. In the third regime, the zone would again be dominated by bubbles that behave much as stable cavities.

An objective of this paper is to seek a dynamical basis for the existence of such thresholds and of the observed maxima in cavitation activity. This paper is the third in a series on cavitation dynamics. In the first⁸, hereinafter referred to as CD:I, a mathematical formulation for predicting the motion of, and other quantities associated with, a small cavity set into motion by an acoustic pressure field in a liquid was derived. This formulation consists of a set of differential, integral and algebraic non-linear equations that take into account compressibility and viscosity of the liquid, heat conduction across the interface and surface tension. The equations have been programmed for solution on a digital computer. In the second paper⁹, hereinafter referred to as CD:II, this formulation was used to study the free pulsations of small argon-filled cavities in water. The results presented in CD:II (and in an expanded report¹⁰) are fundamental to the interpretation of calculations reported here.

The limitations on the usefulness of such a mathematical model include the assumptions that the speed of sound in the liquid is constant (that is, the variational pressure is a linear function of the variational density), that the cavity retains its spherical shape throughout its motion, that the amount of gas in the cavity remains constant and that the gas in the cavity behaves as an ideal gas.

In the calculations reported here, a pre-existing seed of argon

in water grows into a cavity under the influence of a uniform, sinusoidal acoustic field characterized by a pressure amplitude, P_A , and a frequency, f_A .

The system of notation adopted in CD:I will be used in this paper. An asterisk (*) is used to denote a quantity in some consistent set or units. In this notation, p^* is a pressure in bars and $p = p^*/p_n^*$ is the non-dimensional pressure where p_n^* is the reference pressure (here taken to be 1 bar). Thus P_A is the non-dimensional pressure amplitude, P_A^*/p_n^* . The quantity $R = R^*/R_n^*$ is the non-dimensional radius of the cavity, R^* its radius in centimeters and R_n^* the initial radius of the cavity in centimeters. The frequency, f , is the non-dimensional frequency $f^*t_n^*$ where f^* is the frequency in Hertz and $t_n^* = R_n^*/a_n^*$ and a_n^* is the equilibrium speed of sound in the liquid.

Once set into motion, the cavity passes through a series of maxima and minima and its motion may or may not be periodic. The complexity of this non-linear motion results from the tendency of the cavity to pulsate both at the driving frequency, f_A , and at some resonance frequency, f_r , of free pulsation as determined in CD:II. When the motion is periodic, there is a least period, T_L , in which the motion repeats itself. This least period, T_L , must be an integral multiple of both the acoustic period, $T_A = 1/f_A$, and the period of free pulsation, $T_r = 1/f_r$; that is, for a periodic motion, $T_L = m T_r = n T_A$ where n and m are integers. Of particular interest is the case where $m = 1$ and $T_L = T_r = n T_A$. The motion is then said to contain a subharmonic order n (or, in terms of frequency, $f_L = f_r = f_A/n$ and there is said to be a subharmonic of order $1/n$).

Most motions of cavities in an acoustic pressure field are quasi-periodic; that is, the radius-time curve shows a slowly varying time interval that approximates a least period, T_L , and the maxima and minima in such a period change slowly in amplitude and phase from one such quasi-period to the next.

The non-linear motion of a cavity is thus a combination of a free pulsation and a driven pulsation, both of which contain a fundamental and associated harmonics. The driven pulsation has the period, T_A , of the acoustic field, but the period of the free pulsation, T_r , depends on the amplitude of motion, as shown in CD:II. In general, in a least period, T_L , the radius time curve will be quite complicated. However, when the amplitude of

motion is such that the period, T_r , of free pulsation equals the acoustic period, T_A , then the motion consists of a single maximum and a single minimum in a least period, $T_L = T_A = T_r$. The frequency f_r at which this coincidence takes place is the non-linear resonance frequency for a cavity of initial radius, R_n^* , in an acoustic field specified by the pair (P_A, T_A) . This non-linear resonance frequency is always less than the linear resonance frequency, f_o , for a cavity pulsating with very small change in radius.

Curves of the resonance frequency, f_r , as a function of the maximum radius, R_o , are shown in Fig. 2 and Reference 10 for various values of initial cavity radius, R_n^* . When a cavity of initial radius, R_n^* , is driven at an acoustic frequency, f_A , these curves tell us the maximum radius, R_o , at which the specified f_A equals some resonance frequency, f_r , of that cavity. In a non-linear pulsation at a frequency close to some f_r , the radius-time curve has an unique maximum, R_o , corresponding to the specified pressure amplitude, P_A . This pressure amplitude at which the acoustic frequency f_A equals a resonance frequency, f_r , will be called the resonance pressure, P_r .

We shall find that the resonance pressure, P_r , determines one cavitation threshold. Another cavitation threshold is defined through use of a function called the dynamical threshold radius, R_t , described in CD:II for free pulsations. When the maximum radius, R_o , of an expanding cavity of initial radius, R_n^* , exceeds the threshold radius, the cavity is a transient cavity. When such a cavity collapses, inertial forces in the surrounding liquid generate rapidly increasing kinetic energy that is either stored in the compressible liquid or converted into internal energy of the cavity contents. Ultimately, the inward motion is halted by the pressure in the cavity and part of the stored energy radiated as a shock wave. Most of the phenomena summed up as cavitation activity are brought about by transient cavities.

Determination of the threshold radius, R_t , requires partition of the acceleration of the cavity interface into two functions: the pressure function, PF, and the inertial function, IF. When a cavity starts to contract from a maximum, R_o , PF first decreases, passes through a minimum and then increases. IF is a function of

the maximum radius, R_0 , at the start of collapse, and the value of R_0 for which IF intersects this minimum is the threshold radius, R_t .

When a cavity of initial radius R_n^* pulsates in an acoustic pressure field of frequency f_A , its maximum radius increases when the pressure amplitude, P_A , increases. The value of P_A which causes R_0 to equal or exceed R_t will be called the threshold pressure, P_t .

It is qualitatively obvious that cavitation activity must increase with acoustic pressure, but must eventually decrease. As the pressure amplitude increases the average volume of a cavity becomes much larger than its equilibrium volume and the cavity spends most of a period, T_L , in such an expanded state. The liquid then becomes much more compressible and this increase in compressibility strongly moderates the violence of collapse. The exciting sound beam is both scattered and absorbed by the increased cross-sections of the cavities and the radiated shock waves from collapsing cavities will likewise be scattered and absorbed by surrounding cavities. Because there may be an enormous number of cavitation events per cm^3 in a cavitation zone, any increase in the average size of cavities may have a drastic effect on cavitation activity. Sirotyuk¹¹ estimates that there may be as many as 10^6 cavitation events per cm^3 .

The mathematical model of CD:I used in carrying out the calculations reported here predict the motion of a single cavity in an infinite, homogeneous liquid. With this restriction in mind, two quantities have been chosen for calculation they might give insight into the thresholds observed in zones containing many bubbles with a wide distribution of initial radii. These quantities are the maximum pressure, p_m , in a collapsing cavity and the work, W_E , done by a cavity on the surrounding liquid in expanding from its minimum radius, R_m , to a maximum radius, R_0 . This work is $W_E = W_E^*/W_n^*$ where $W_n^* = 0.88 \text{ kJ mol}^{-1}$.

The maximum pressure, p_m , determines the initial strength of the radiated shock from a collapsed cavity and W_E measures the transfer of energy to the liquid by the compressed gas in the cavity. In any expansion, most of the work, W_E , is done in the initial stage when R is close to R_m . Thus, while p_m determines the strength of the shock front, W_E determines the width and magnitude of the

shock wave behind the front. Because the least period T_L , may be many times the acoustic period, T_A , the work, W_E , is here defined as the average work done by an expanding cavity in an acoustic period, T_A , the average being taken over values in the least period, T_L .

Fig. 1 shows the maximum pressure, p_m^* , predicted for a cavity of initial radius $R_n^* = 5 \times 10^{-4}$ cm. as a function of the acoustic pressure amplitude, P_A^* , for three frequencies of the acoustic field. These frequencies, 600 kHz, 300 kHz, and 100 kHz, are approximately equal to f_0 , $f_0/2$ and $f_0/6$ where f_0 is the linear resonance frequency of the cavity.

At the calculated threshold pressure, P_t , there is a marked change in the maximum pressure at 300 kHz and 100 kHz. At 600 kHz the inertial function IF always lies above the minimum in PF and P_t is undetermined.

We can draw two conclusions from the location of the resonance pressure, P_r , on these curves. Most points on these curves are accompanied by an integer. This integer indicates the least period in terms of T_A . Thus $n = 1$ means $T_L = T_A$, while $n = 4$ means that $T_L = 4 T_A$ and a subharmonic of order $1/4$ exists. The location of P_r divides each curve into two parts. Below P_r only one subharmonic could be found, while above P_r there exists a profusion of subharmonics of various orders. At 300 kHz and 100 kHz, the curves of p_m^* abruptly decrease in slope in the vicinity of P_r , but at 600 kHz the change in slope is much less marked.

Fig. 3 shows the maximum pressure, p_m^* , as a function of the acoustic pressure amplitude, P_A^* , for three different cavities. Each cavity is driven at a frequency equal approximately to $f_0/2$ corresponding to its initial radius, R_n^* . On all three curves the threshold pressure, P_r , marks an abrupt change in the slope of the curve and in the vicinity of the resonance pressure, p_r , there is an even more pronounced decrease in the slope of p_m^* as a function of P_A^* . Again, there are subharmonics in abundance above P_r but only one below it.

The maximum pressure curves would lead us to identify P_t with the first cavitation pressure threshold of Monakhov et al and the resonance pressure, P_r , at which $f_A = f_r$ with the second cavitation pressure threshold. At P_r the maximum radius, R_0 , is

the resonance radius for the driving frequency, f_A . These conclusions would appear to apply only to cavities driven at frequencies well below the linear resonance frequency, f_0 .

The work, W_E , per T_A done by an expanding cavity is shown in Fig. 4 as a function of the acoustic pressure amplitude, P_A^* , for a cavity of initial radius, $R_n^* = 5 \times 10^{-4}$ cm. For this calculated quantity it is even clearer that P_t and P_r are the first and second pressure thresholds, at least for f_A much less than f_0 .

Fig. 5 shows W_E as a function of P_A^* for three different cavities. Each cavity is driven at a frequency f_A approximately equal to $f_0/2$. For each cavity, P_r is the pressure threshold at which there is a marked decrease in the slope of the curves. For the 5×10^{-5} cm. cavity, P_t does not appear to act as a threshold while the point at $P_A^* = 4$ bars does. The significance of this remark lies in the fact that, at this pressure, a quantity called the energy dissipation modulus, $\Delta W/W_m$, defined in CD:II, is a maximum. Again, in the curves for W_E , subharmonics appear in general only above the second threshold, P_r .

The calculations reported here predict the behavior of a single bubble in an infinite, homogeneous liquid, and one must be cautious in seeking quantitative correspondences with experimental results, which in general are statistical averages over many bubbles. The maxima characteristic of cavitation activity do not appear, nor should we expect them to. However, the results clearly give us useful insights into experiments such as those of Monakhov et al. Thus, despite these restrictions, there are several general remarks that can be made about the results reported in this paper:

1. The quantity, P_t , is a pressure threshold at which cavitation actively rapidly increases for any driving frequency, f_A , well below f_0 , the linear resonance frequency of a cavity. Tentatively, P_t may be identified as the first cavitation threshold of Monakhov et al.
2. On the other hand, P_t does not appear to be a cavitation threshold when f_A is approximately equal to f_0 or R_n^* is less than a micron. When R_n^* is less than a micron, the first cavitation

threshold may occur when the energy dissipation modulus, $\Delta W/W_m$ is a maximum, as suggested in CD:II.

3. A second pressure threshold, P_r , occurs when the driving frequency, f_A , equals a non-linear resonance frequency, f_r , of the cavity. Tentatively, P_r may be identified with the second threshold of Monakhov et al.

4. At the second threshold, P_r , both the maximum pressure and W_E change abruptly for driving frequencies less than the linear resonance frequency of the cavity. Curves of both maximum pressure and W_E tend to flatten out for pressure amplitudes greater than P_r . Changes in the medium due to expanded cavitation bubbles, noted above, may cause these curves to decrease above P_r .

5. Subharmonics in general are present only in the region above the second threshold, P_r , which may be identified as the region of reduced cavitation activity defined by Monakhov et al.

6. Cavities with initial radii greater than a micron are more effective in producing cavitation activity when driven at frequencies less than their linear resonance frequencies.

REFERENCES

1. L. D. Rozenberg, "La generation et l'étude des vibrations ultrasonores de très grande intensité," *Acustica* 12, 40-49 (1962).
2. H. G. Flynn, "Physics of Acoustic Cavitation in Liquids," in *Physical Acoustics*, Vol. 13 (W. P. Mason, ed.), Academic Press, New York, 1964.
3. Gary E. Kaufman, Morton W. Miller, T. Dan Griffiths, Victor Ciaravino, Edwin L. Carstensen, "Lysis and viability of cultured mammalian cells exposed to 1 MHz ultrasound," *Ultrasound in Med. and Biol.* 3, 21-25 (1977).
4. P. R. Clark and C. R. Hill, "Physical and chemical aspects of ultrasonic disruption of cells," *J. Acoust. Soc. Am.* 47, 649-653 (1969).
5. E. A. Neppiras and W. T. Coakley, "Acoustic cavitation in a focused field in water at 1 MHz," *J. Sound and Vibration* 45, 341-373 (1976).
6. V. N. Monakhov, S. L. Peshkovskii, A. S. Popovich, B. I. Fomichev, I. P. Chinyakov and A. D. Yakovlev, "Second ultrasonic cavitation threshold in water," *Soviet Physics-Acoustics* 21, 268-269 (1975).
7. N. B. Brandt, A. D. Yakovlev and S. L. Peshkovskii, "Second Threshold for Cavitation," *Sov. Tech. Phys. Lett.* 1, 212-213 (1975).
8. H. G. Flynn, "Cavitation dynamics: I. A mathematical formulation," *J. Acoust. Soc. Am.* 57, 1379-1396 (1975).
9. H. G. Flynn, "Cavitation dynamics: II. Free pulsations and models for cavitation bubbles," *J. Acoust. Soc. Am.* 58, 1160-1170 (1975).
10. H. G. Flynn, "Cavitation dynamics: II. Free pulsations and models for cavitation bubbles," report of Acoustical Physics Laboratory, University of Rochester, 1972.
11. M. G. Sirotyuk, "Energetics and dynamics of the cavitation zone," *Soviet Physics-Acoustics* 13, 226-229 (1967).

FIGURES

- Fig. 1 Maximum pressure in a 5-micron cavity
- Fig. 2 Non-linear resonance frequency curve for a 5-micron cavity
- Fig. 3 Maximum pressure in three cavities
- Fig. 4 Work, W_E , done by an expanding 5-micron cavity
- Fig. 5 Work, W_E , done by three expanding cavities

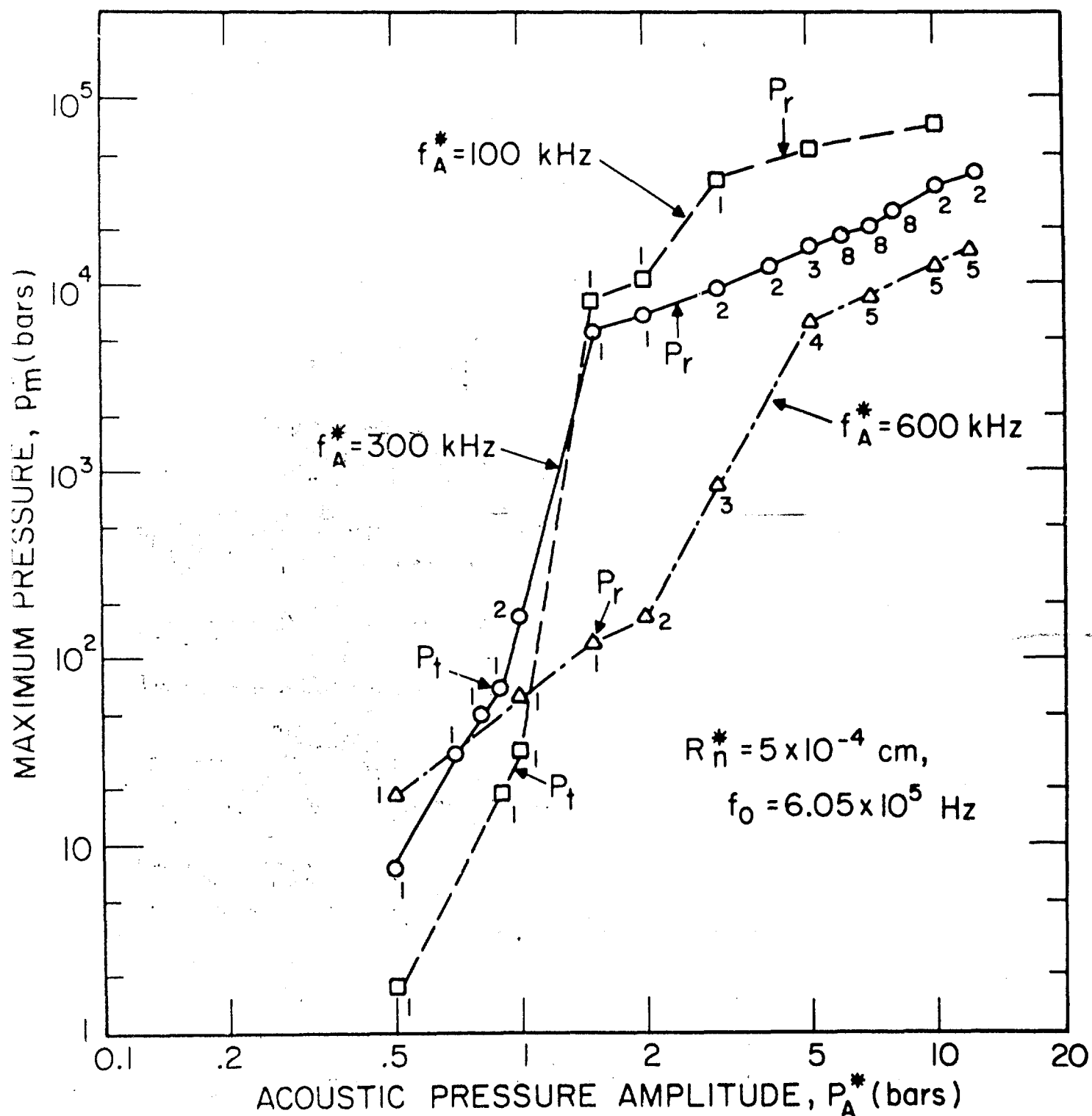


Fig. 1 Maximum pressure in a 5-micron cavity
 PRECEDING PAGE BLANK

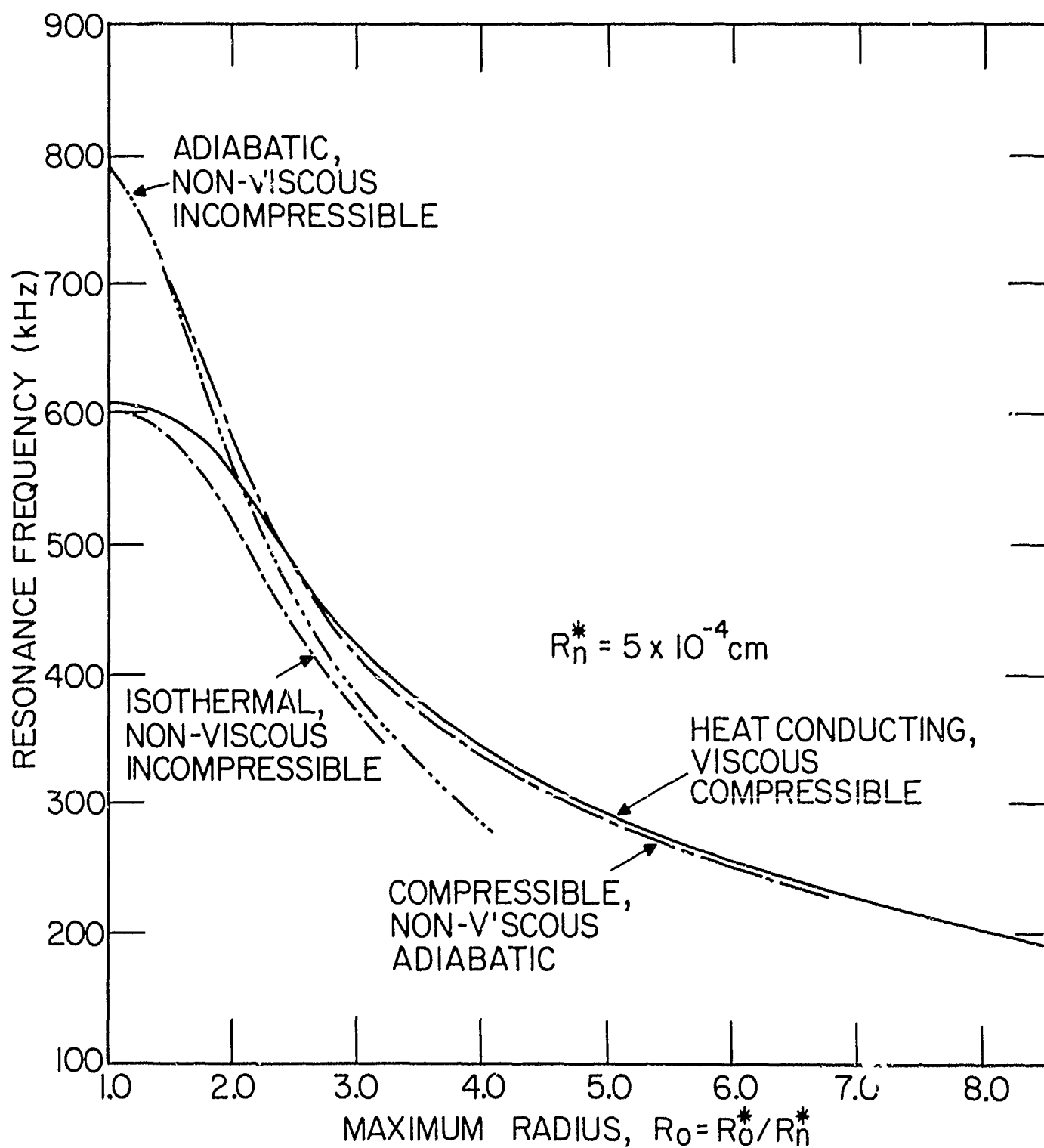


Fig. 2 Non-linear resonance frequency curve for a 5-micron cavity

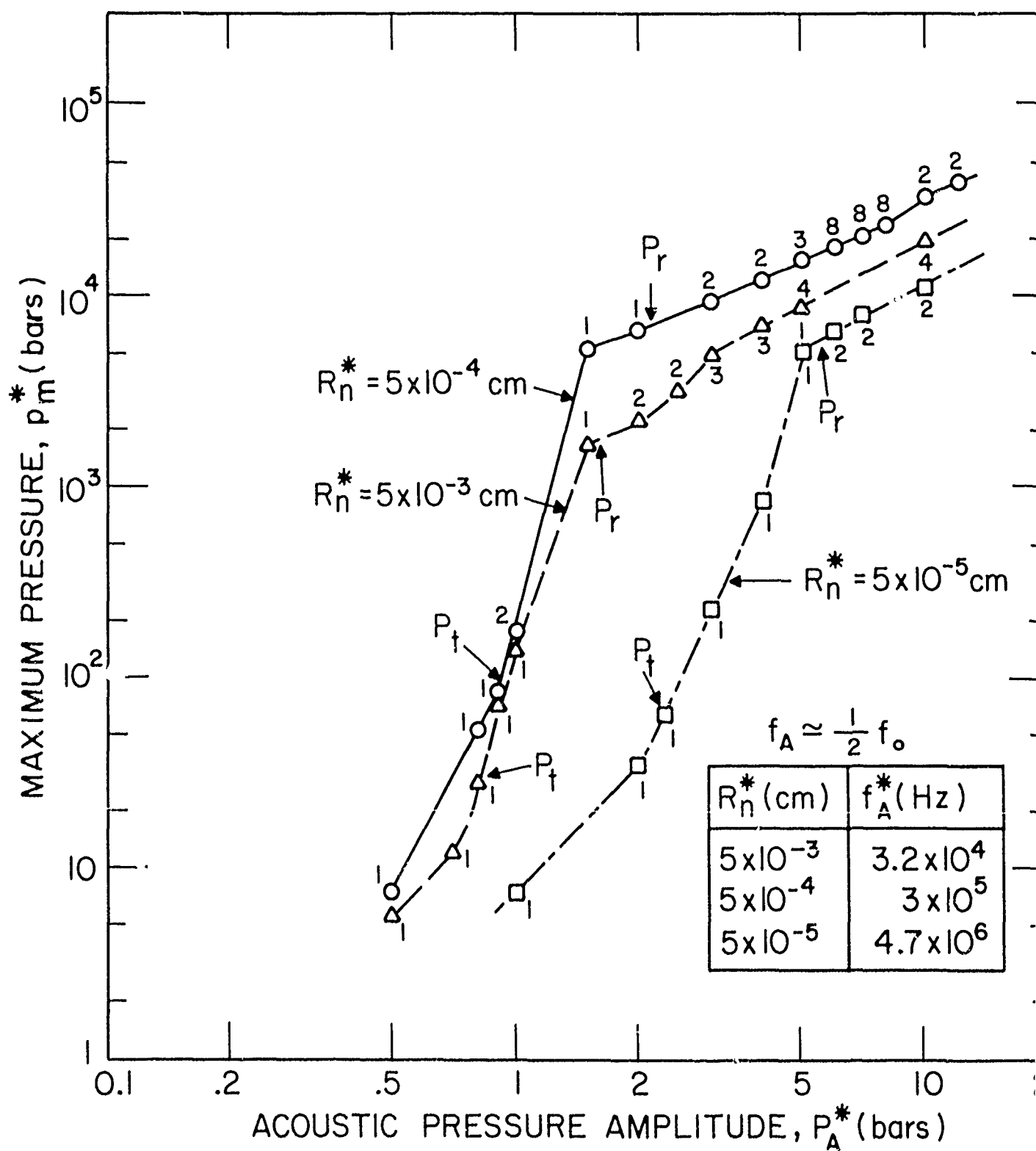
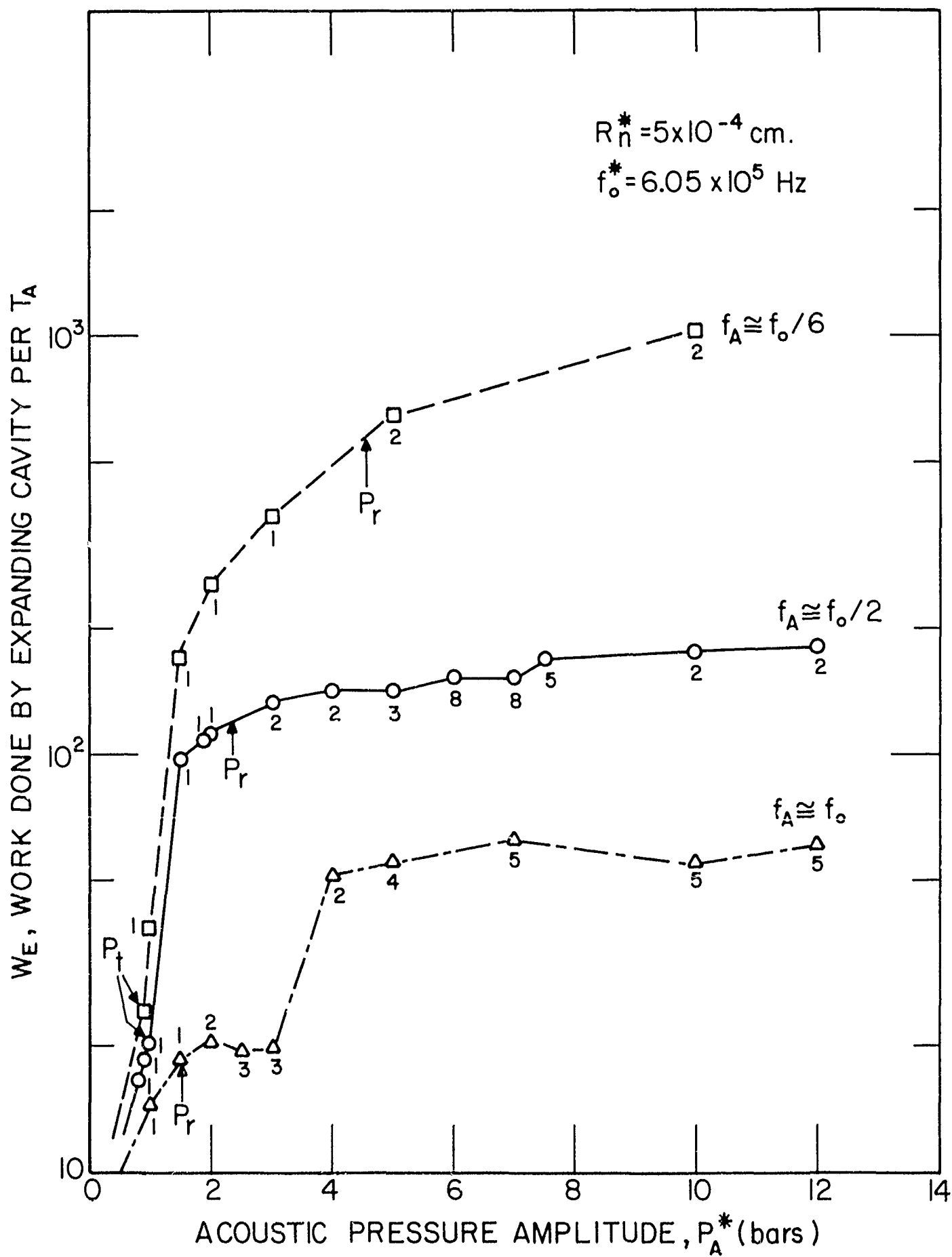


Fig. 3 Maximum pressure in three cavities



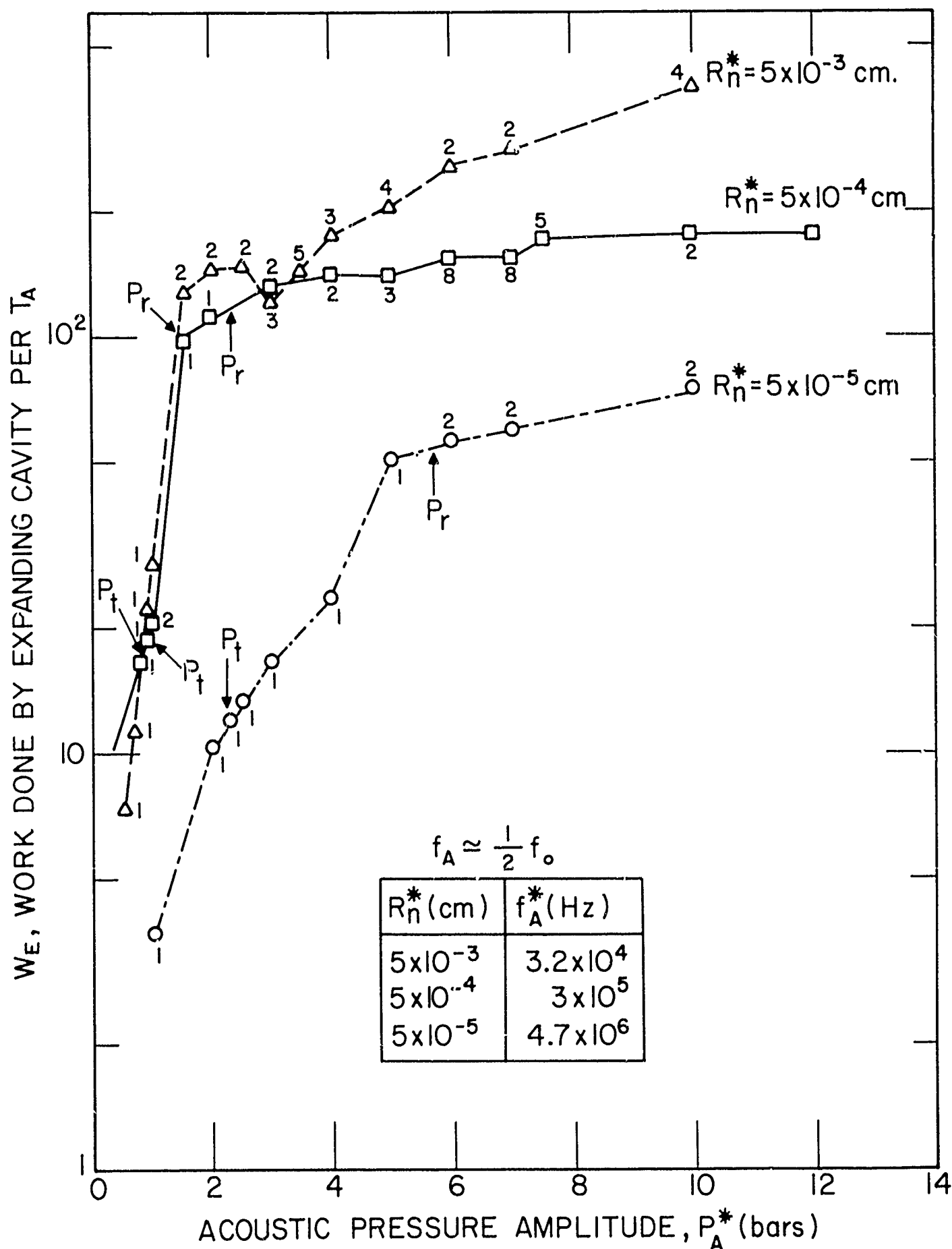


Fig. 5 Work, W_E , done by three expanding cavities